

# IASING science data processing overview

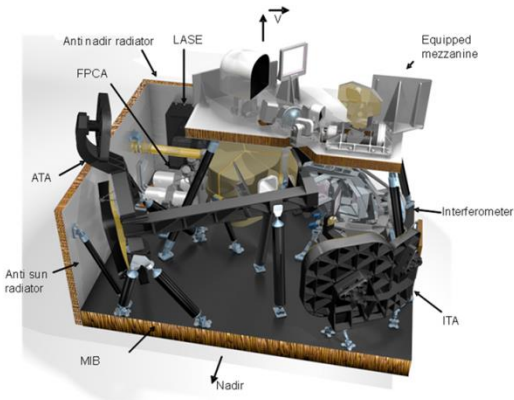
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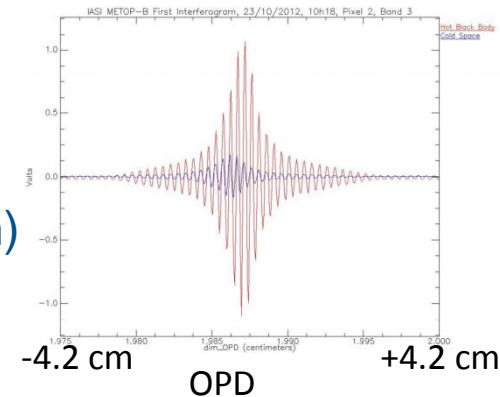
# Introduction



- IASI-NG instrument measures interferogram (not spectrum !)

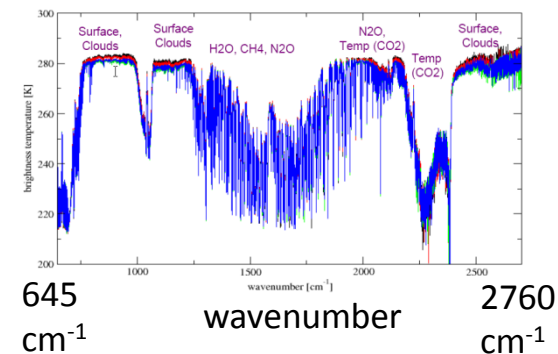
- Interferogram = Fourier Transform (Spectrum)

Note : all these data are sampled data, not continuous !



- Users work with L1C spectrum (+ additional information like flags, cloud fraction,....)

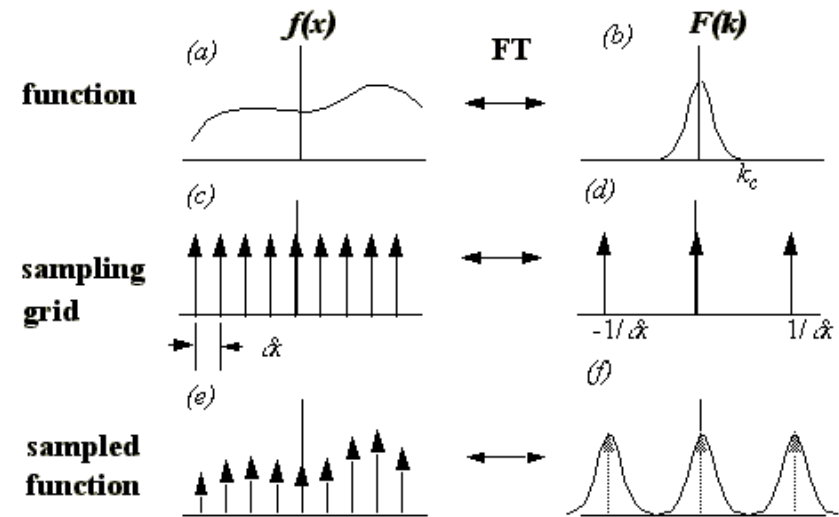
- L1C spectrum (“user friendly approach”)
  - ◆ fully calibrated (spectral and radiometry)
  - ◆ a unique ISRF for all channels of all spectra
  - ◆ a sounding is a geo-localized point
  - ◆ performance requirement : Radiometry = IASI / 2, Spectral = IASI/2, geometry = IASI



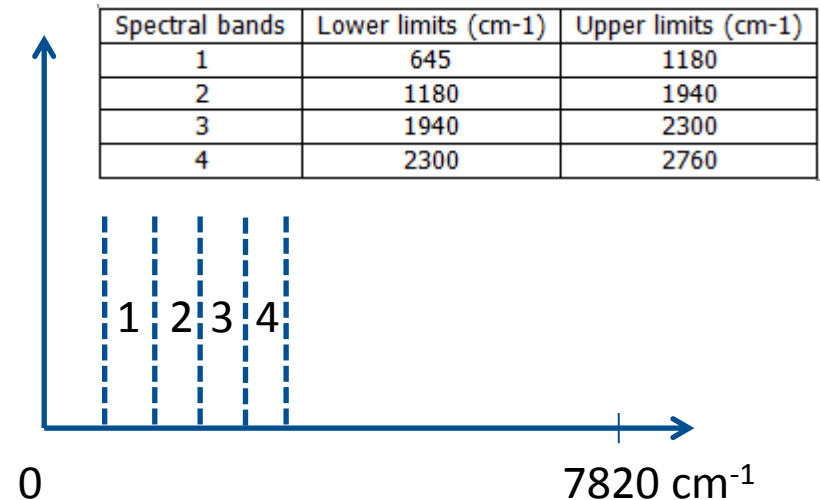
On-board/ground sharing is driven by TM allocated (6 Mb/s in average, excluding a sub-set of full measured interferogram verification data.)

# On-board processing objectives

- As long as interferogram acquisition and sampling is done properly (Shannon criteria respected and anti-aliasing filter), **all the meaningful information is contained in  $[0, v_s/2]$** , where  $v_s$  is the wavenumber associated to the sampling frequency ( $v_s/2 \sim 7820 \text{ cm}^{-1} = 1.2788 \mu\text{m}$ )

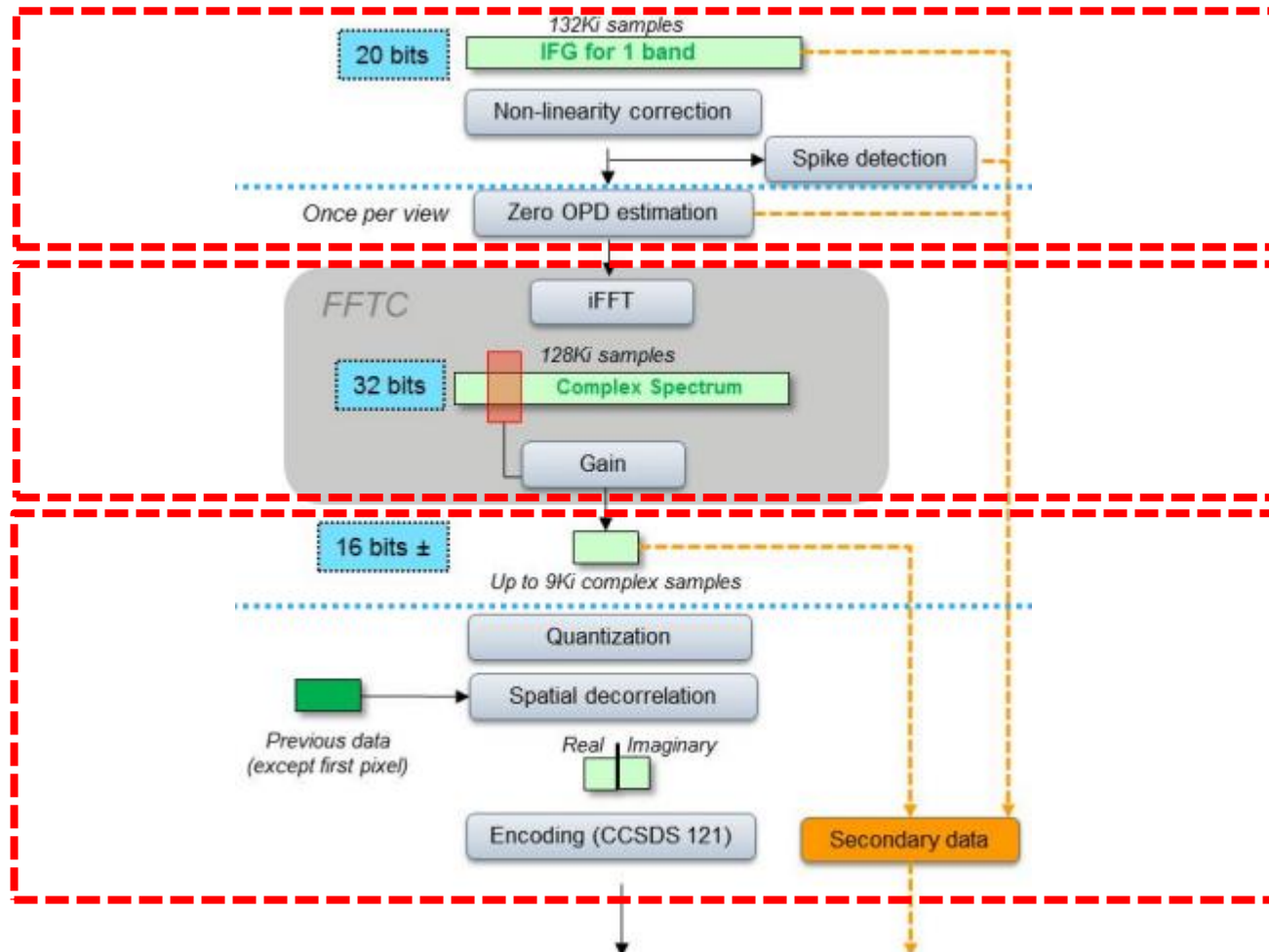


- The logic of the design becomes then more obvious
  - ◆ Preserve the information content by keeping the Fourier transform reversible in the useful spectral band and with respect to instrument artifacts we correct on ground
  - ◆ Be compliant with computation time and telemetry data rate.
  - ◆ The data flow is compressed from 200 Mb/s to 6 Mb/s !



# On-board processing of science data

16 (pixels) x 4 (bands) sampled interferograms



16 (pixels) x 4 (bands) compressed complex spectra  
(real + imaginary parts)

## Preprocessing

(to avoid spectral aliasing introduced by discrete FT and loss of information)

## 1<sup>st</sup> level of compression

- 1) FFT of interferogram
- 2) Frequency truncation to useful band

(+ interbands + ghost + spikes + monitoring frequencies)

Data rate / 20-25

## 2<sup>nd</sup> level of compression

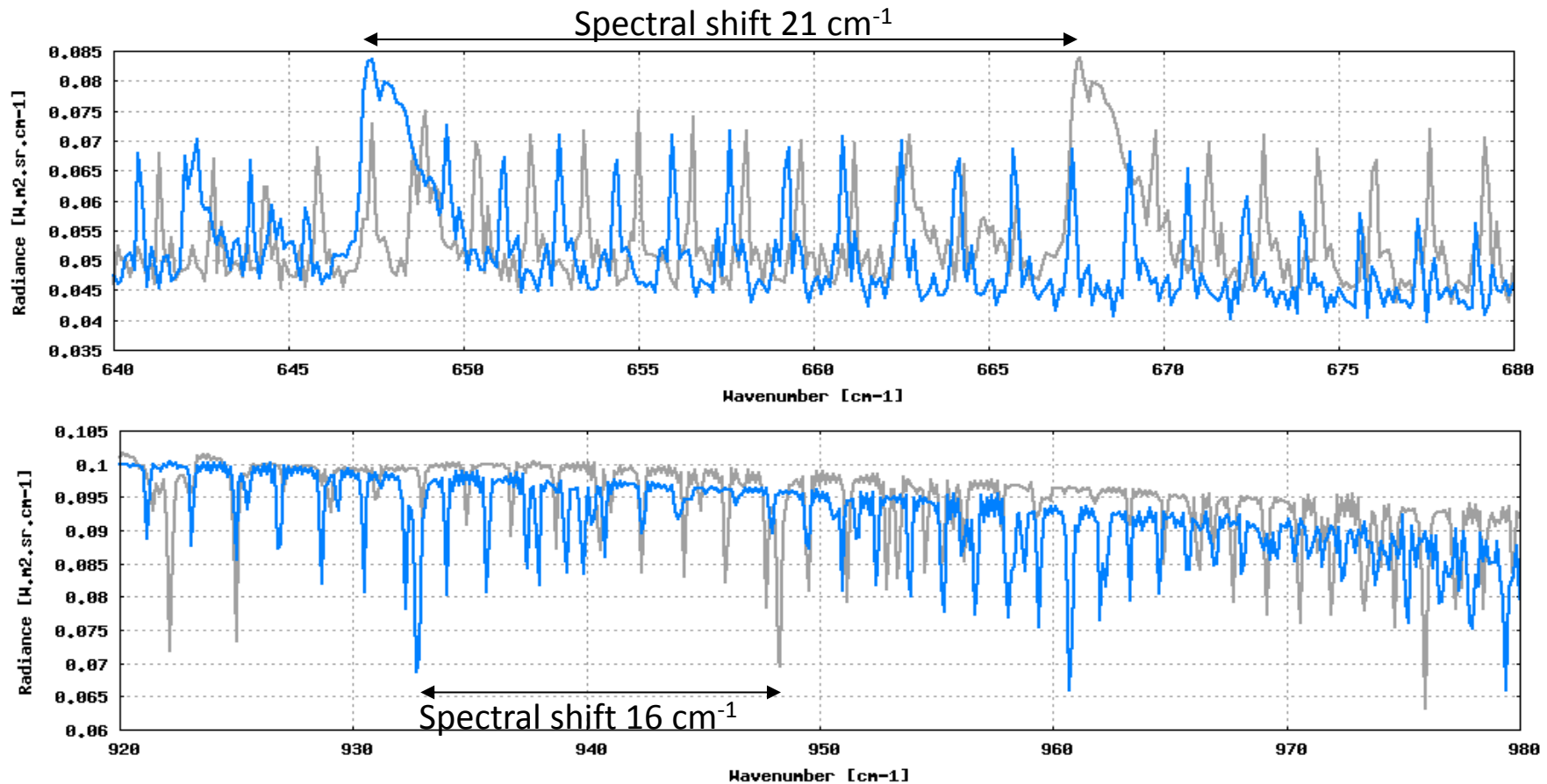
“conventional compression”  
Quasi-loss less (quantization 0.5% noise increase)

Data rate / 2-3

# Space segment output

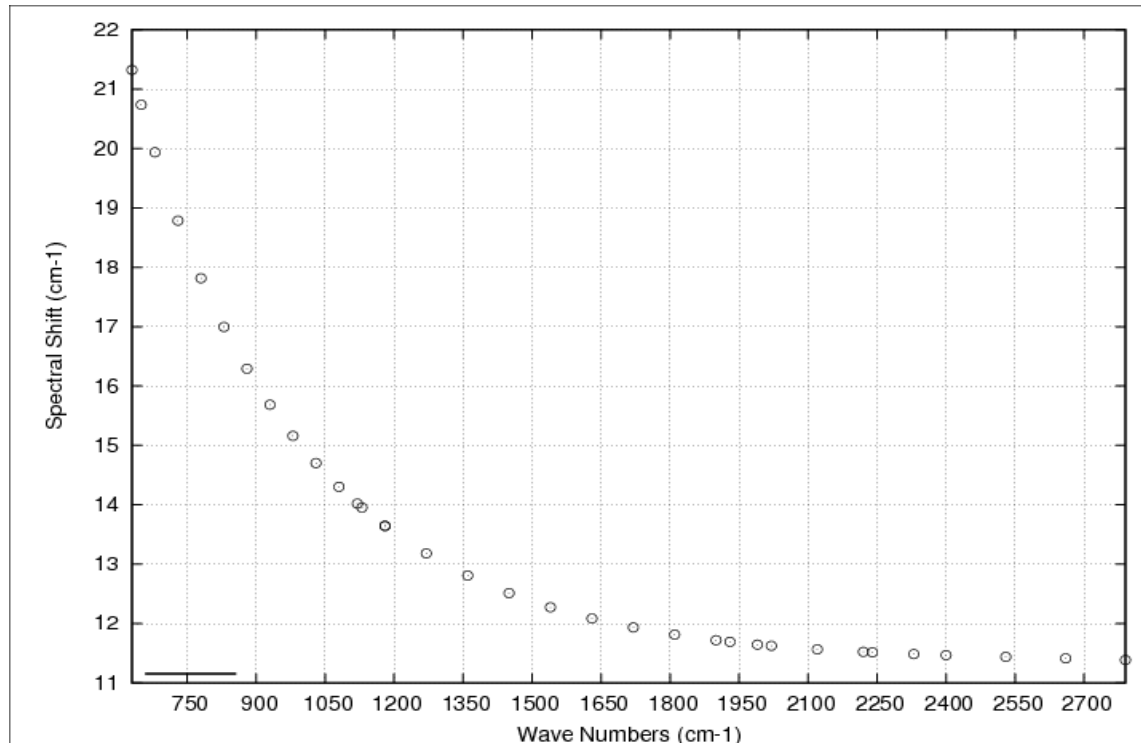
Grey: Atmospheric input spectrum ( $\text{Opd}_{\text{Max}} = 4.2 \text{ cm}$ , SRF = Cardinal sine)

Blue: L0 spectrum space segment output (real part,  $\text{Opd}_{\text{Max}} = 4.2 \text{ cm}$ , SRF = Nominal instrument, Background at 80 K)



# Instrument chromatic spectral shift

- The field compensation within the interferometer is compulsory in order to achieve NedT and spectral resolution requirements
- This field compensation introduces a large chromatic effect (up to  $21 \text{ cm}^{-1}$  @  $645 \text{ cm}^{-1}$ )
- This is a new feature with respect to IASI first generation
- It is corrected by the L1 processing



# On-Ground Processing: objectives

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- Objectives

- ◆ Providing atmospheric **spectra fully calibrated** (spectral and radiometry) and geo-localized
- ◆ Performing **ISRF removal** (de-convolution). The variable ISRF with respect to channel, pixel and time is replaced by a single and standard spectral response function.
- ◆ Providing **additional geophysical characteristics of the scene** (at pixel and sub-pixel scale) in order to help with the exploitation of IASI-NG spectra.
- ◆ Making the **processing in near real time** (more than 1 million spectra per day !)

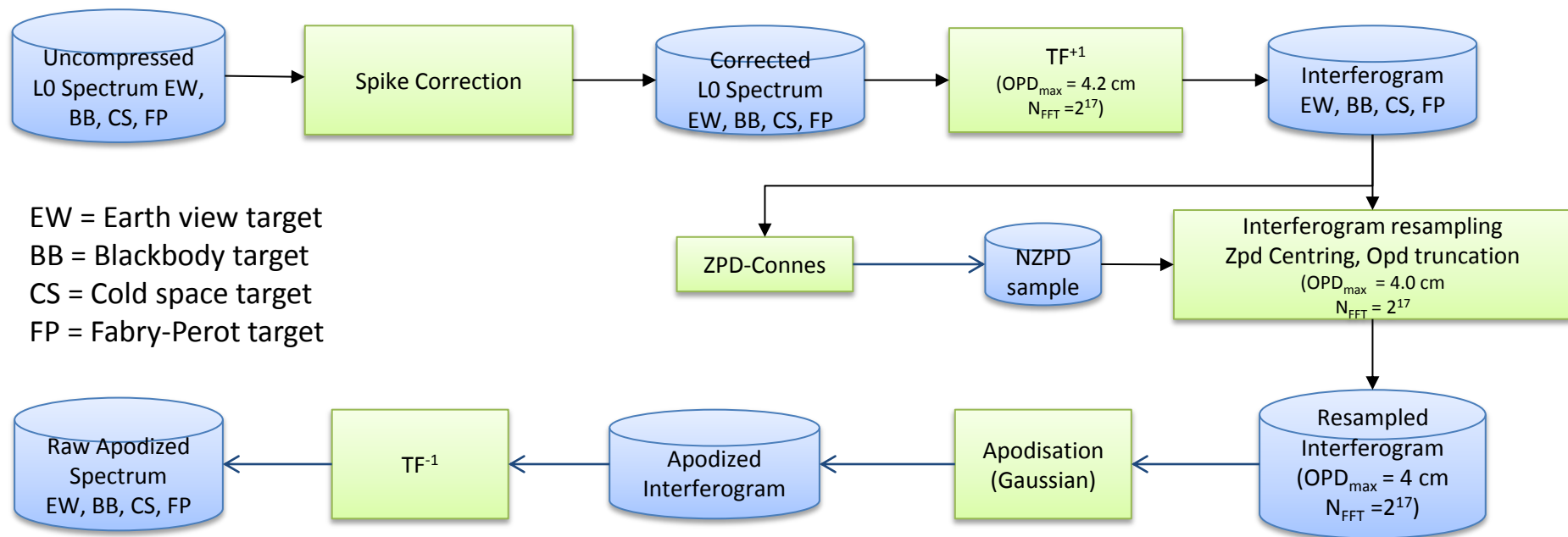
- The main design drivers are

- ◆ ISRF Estimation Model reliability and accuracy
- ◆ Radiometric, spectral and geo-location performances
- ◆ Computing time

# On-Ground Processing: pre-processing (overview)

Pre-processing is mainly done in the interferogram space

Operations: Spike Correction, Direct Fourier Transform, Interferogram Resampling (centered on ZPD), Interferogram Apodisation and Inverse Fourier Transform

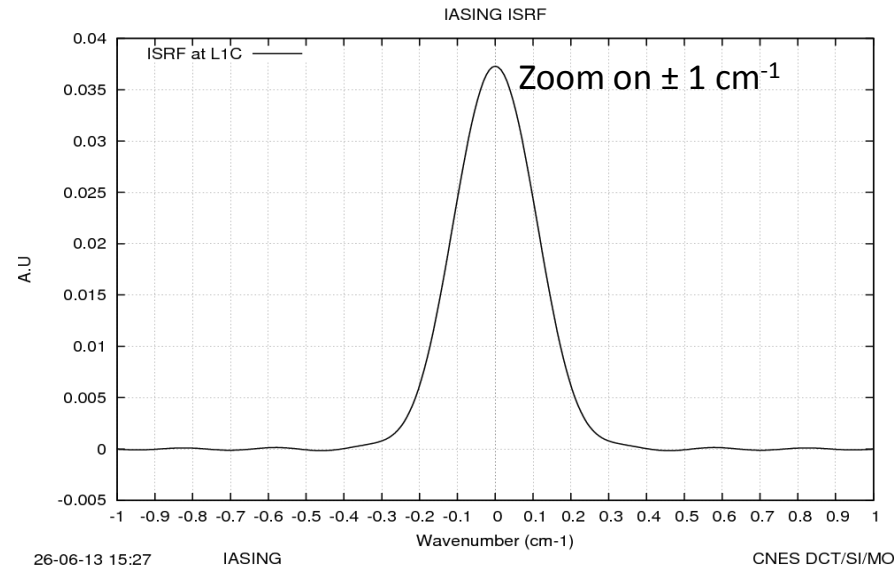


LO and Apodized Raw spectra: reduced to the useful spectral band and complex, intermediate interferograms: real



# On-Ground Processing: pre-processing (apodisation)

- ◆ Numerical apodisation  $I_{ap}(x) = I(x)A_p(x)$
- ◆ Truncated Gaussian: FWHM  $0.25 \text{ cm}^{-1}$  & sampling  $0.125 \text{ cm}^{-1}$  ( $\text{OPD}_{\text{max}}=4 \text{ cm}$ )



- ◆ Fully reversible
- ◆ Can be changed easily (note that improving spectral resolution increases the noise)
- ◆ Making the apodisation before or after the ISRF removal has no impact on spectral performances as long as the apodisation function is symmetric
- ◆ Making apodisation and spectral calibration before the radiometric calibration is compulsory to achieve performance

# On-ground processing: spectral and radiometric calibration

Main-processing is done in the spectrum space

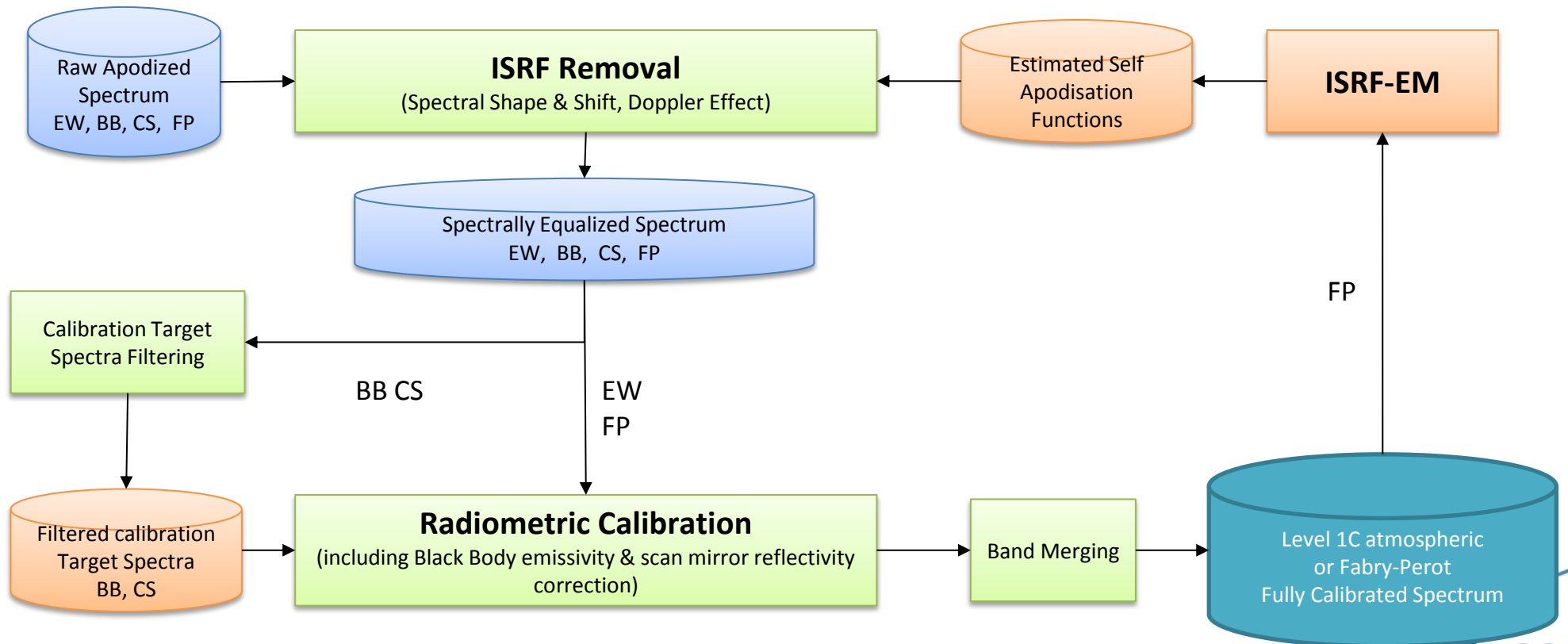
Self Apodisation Functions: complex

Equalized Spectra: complex

Level 1C Spectra:

Real Part disseminated to the users

Imaginary Part delivered to the Technical Expertise Center (TBC)



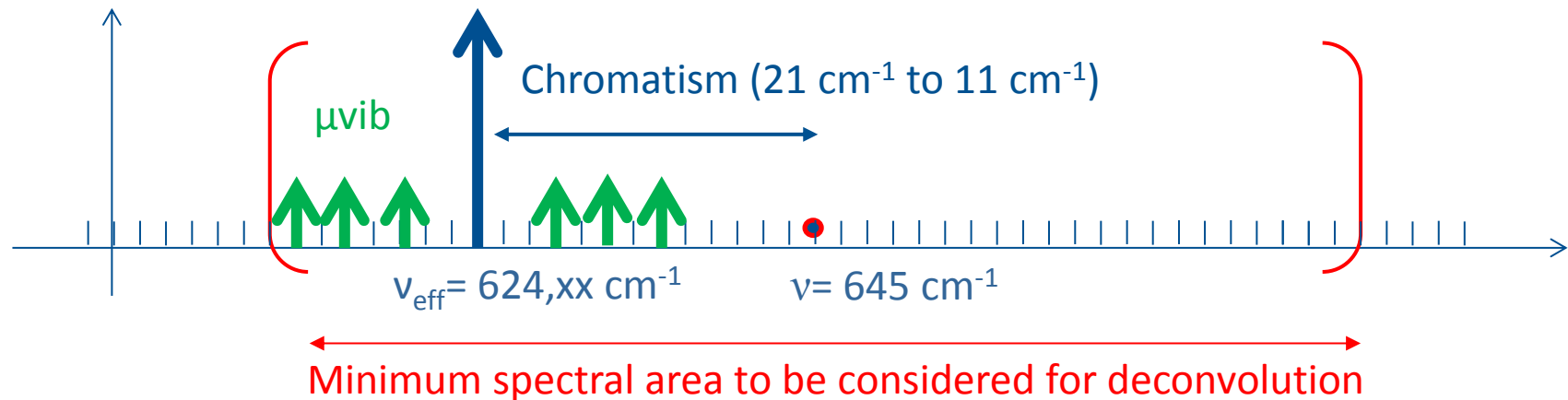
# ISRF removal

- Spectral calibration objectives

- ✦ Correcting from the ISRF centroid shift and shape for each wavenumber

- Spectral calibration principle

- ✦ Monochromatic local deconvolution of the ISRF. As convolution (resp. deconvolution) is a product (resp. division) in the interferogram space, it makes mathematical operations easiest and reversible.
- ✦ “short FFT” of typically  $\pm 512$  or 1024 samples save a huge amount of computing time

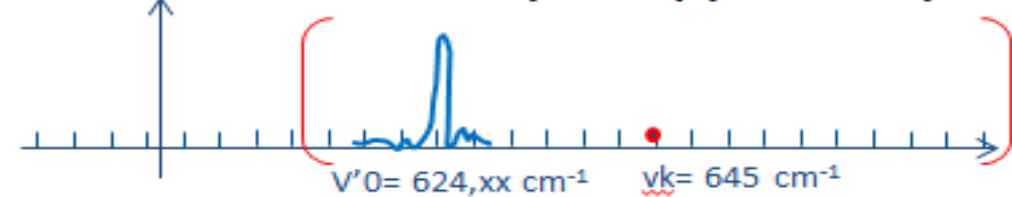


# ISRF removal

Instrument input (spectrum space)



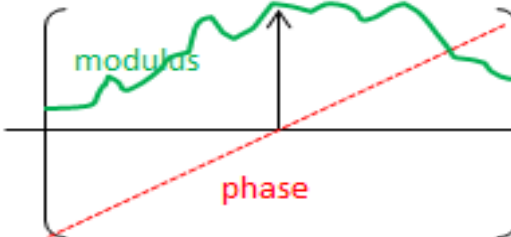
Instrument output L0 (spectrum space)



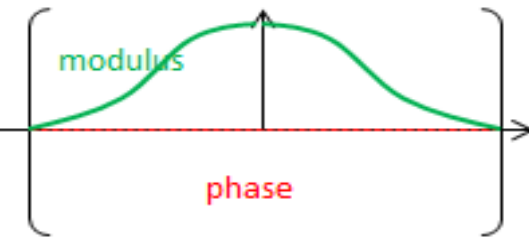
ISRF-EM

Estimated Self Apodisation Functions

Before SAS removal  
(interferogram space)



After SAF removal  
(interferogram space)

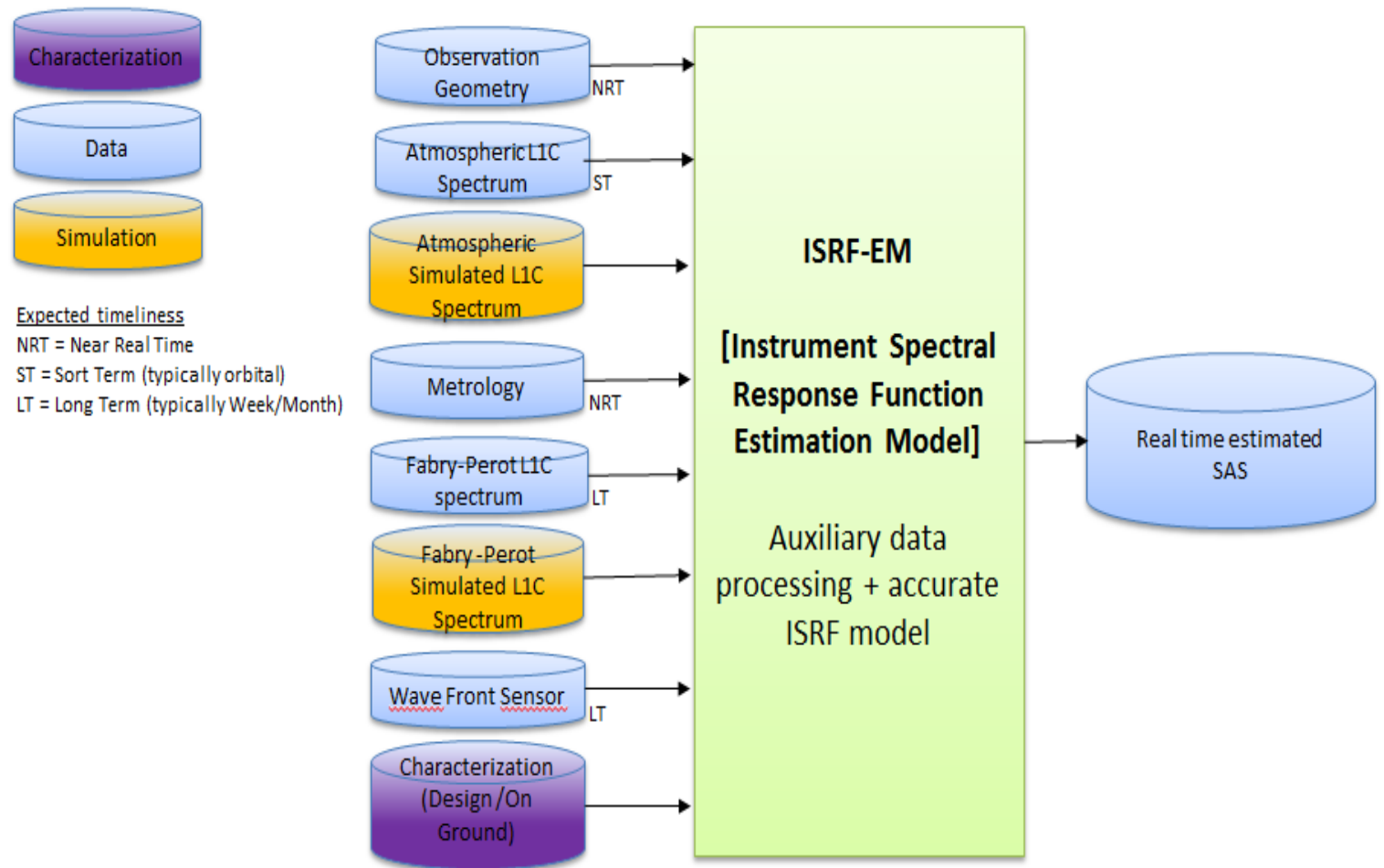


ISRF removal output L1C (spectrum space)



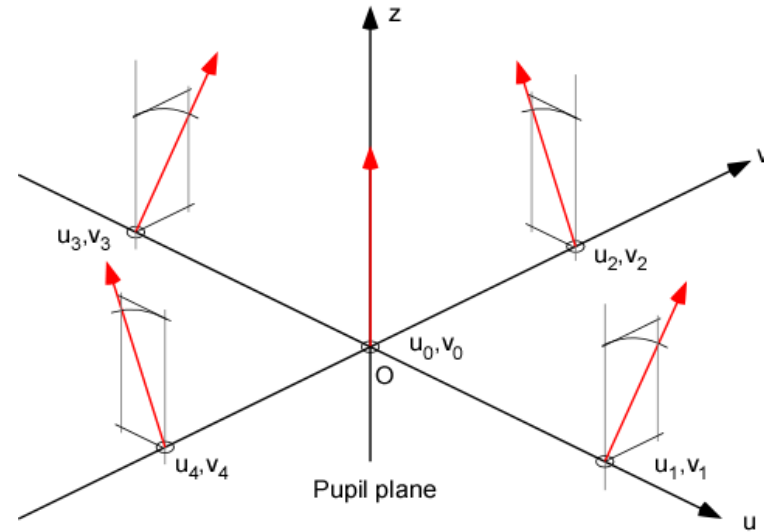
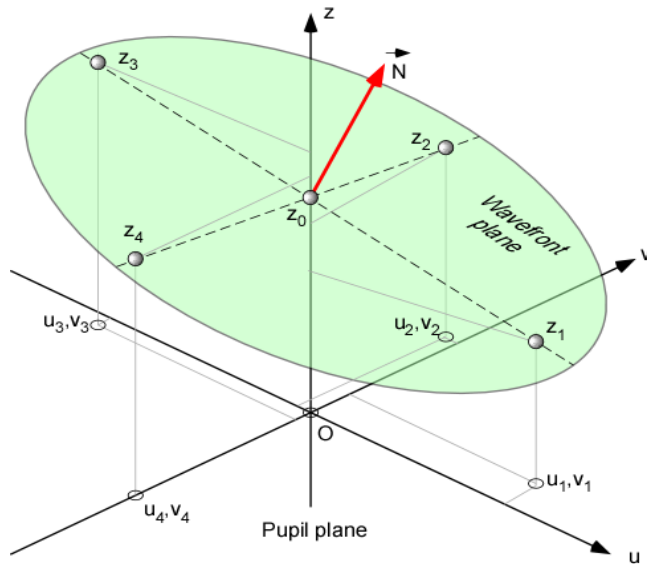
# ISRF-EM objectives

The quality of the ISRF removal relies on an accurate ISRF model + on-ground and in-flight characterisations of input parameters of this model



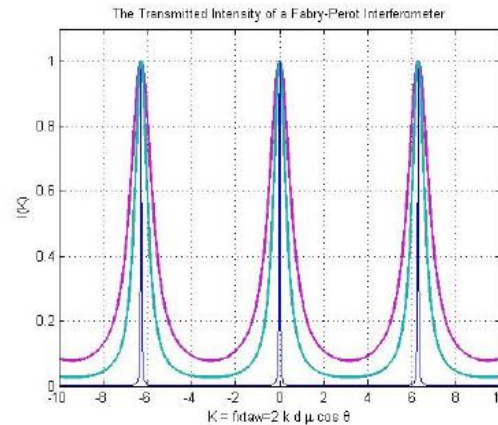
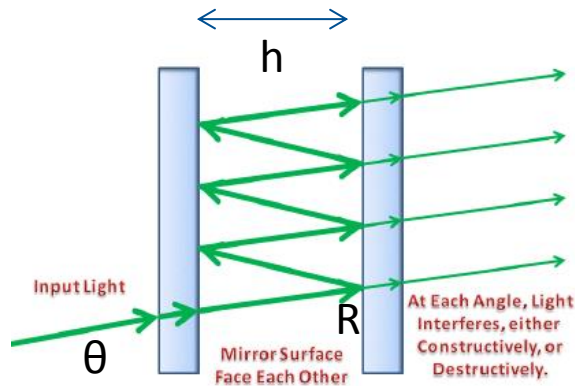
# ISRF-EM Parameter Estimation (Metrology)

The interferometer baseline design includes 5 laser beams



- The on-axis beam  $z_0$  provides the nominal OPD including  $\mu$ vibration effects
- The difference between  $z_2$  &  $z_4$  provides the tilt around  $u$
- The difference between  $z_1$  &  $z_3$  provides the tilt around  $v$
- The mean value of  $z_1$ ,  $z_2$ ,  $z_3$  and  $z_4$  compared to  $z_0$  provides the air/glass ratio
- The difference between the mean value of  $z_2$  &  $z_4$  and the mean value of  $z_1$  &  $z_3$  provides the prism gap

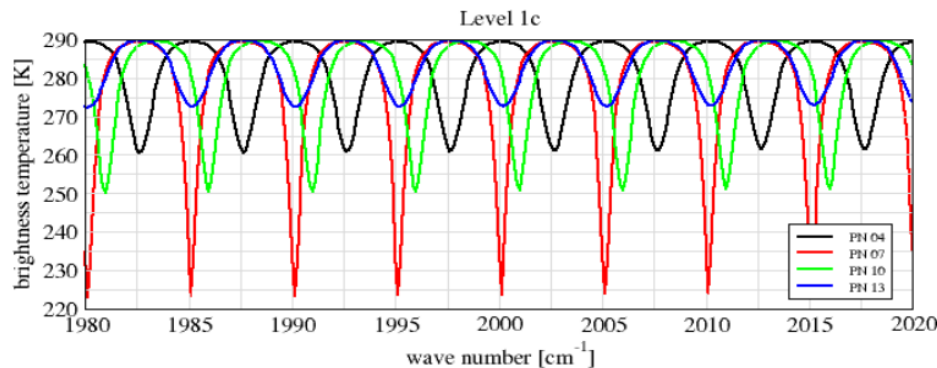
# ISRF-EM Parameter Estimation (Fabry Perot)



$$T_{\text{FPI-0}}(\nu) = \frac{1}{1 + F \cdot \sin^2(2\pi \cdot h \cdot \cos \theta \cdot \nu)}$$

$$F = \frac{4 \cdot R}{(1 - R)^2}$$

- The interferometer baseline design includes a FP device to monitor in-flight IASI-NG spectral calibration (mainly KBr refractive index in the whole spectral domain)
- Signal = reflection of the hot parts of the instrument (including field effect integration and SRF convolution)



FPI level 1c spectra in the spectral range 1980-2020 cm<sup>-1</sup> for detectors 4, 7, 10, and 13

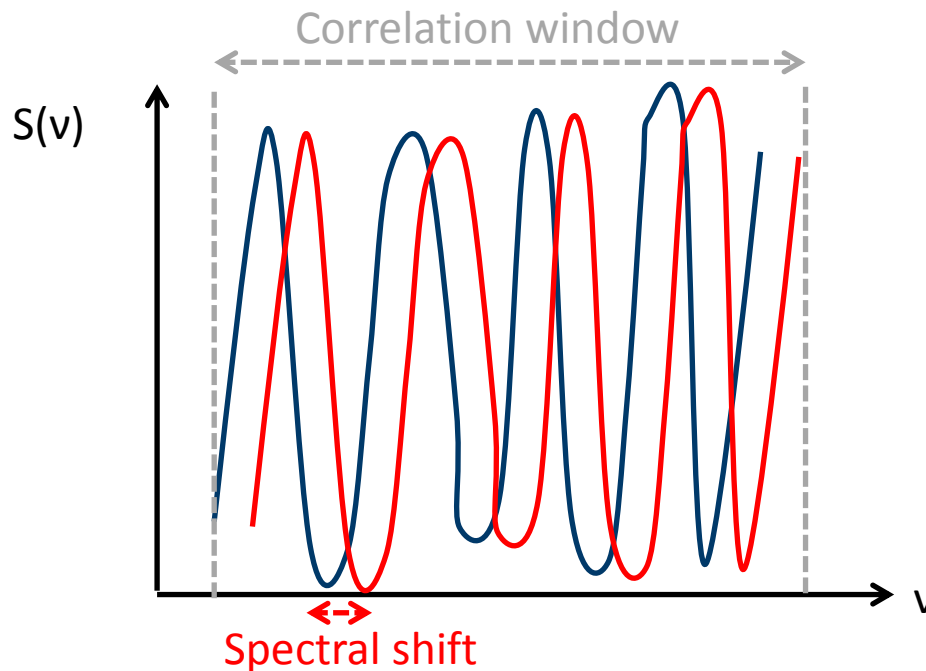
## ● Main advantages

- ◆ it creates a regular spectral pattern that is easiest to model than the atmosphere in the whole spectral range

=> Accurate monitoring of spectral calibration

# ISRF-EM Parameter Estimation (Fabry-Perot)

- Absolute spectral shift is measured through the recognition and accurate location of well-defined patterns in the atmospheric spectrum. It has a strong heritage from IASI first generation.



Measured spectrum  
Simulated spectrum

Fabry-Perot direct model input  
parameters tuning using a set  
of anchor wavenumbers

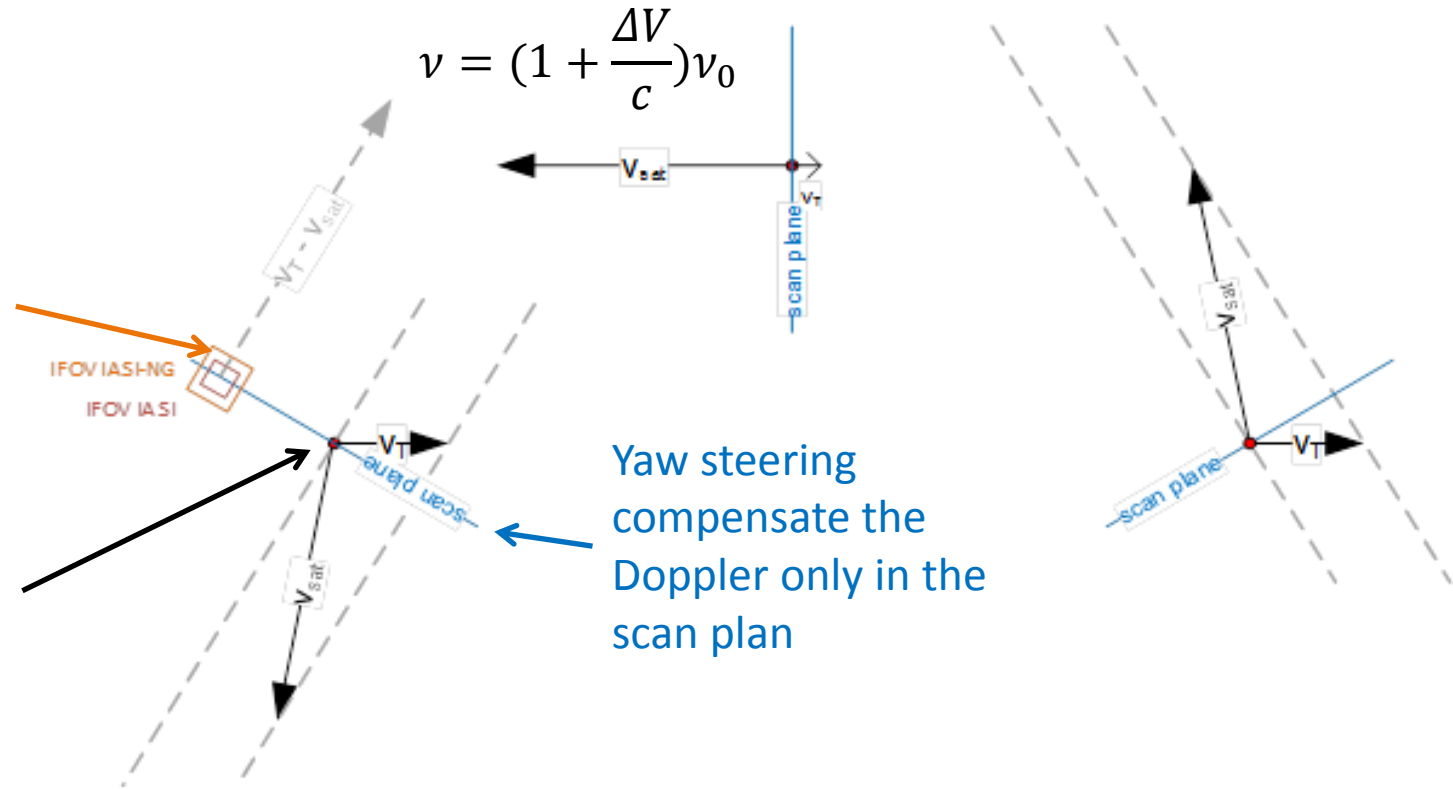
- Algorithms are based on searching for the maximum of correlation between a measured and simulated spectrum (RTM)



# ISRF-EM Parameter Estimation (Doppler shift)

Earth rotation and  
FOV spatial  
extension (max at  
the edge of the  
swath)

LOS stabilization  
during acquisition  
(max at nadir)



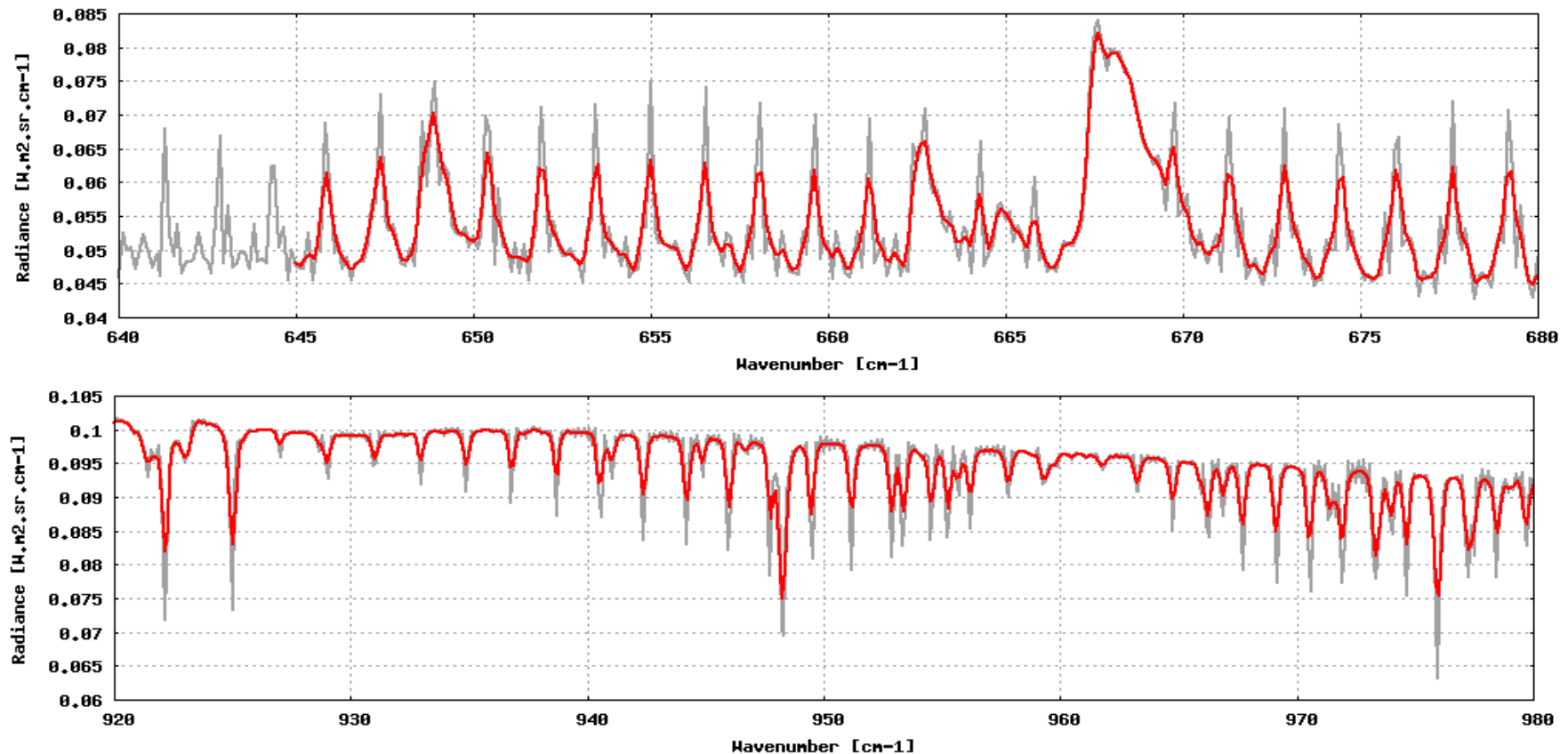
- Residual Doppler shift is not negligible with respect to IASI-NG spectral shift performance (whereas it was the case for IASI)
- Correction using a polynomial variation of SAF phase with respect to  $v$  (expected linear)

$$v_{Dop}(x) = V_{Dop}(@ZPD) + a_{Dop}(1) \cdot x + \sum_{k=2}^{N_D} a_{Dop}(k) \cdot x^k$$

# Ground segment output

Black: Atmospheric input spectrum ( $\text{Opd}_{\text{Max}} = 4.2 \text{ cm}$ , SRF = Cardinal sine)

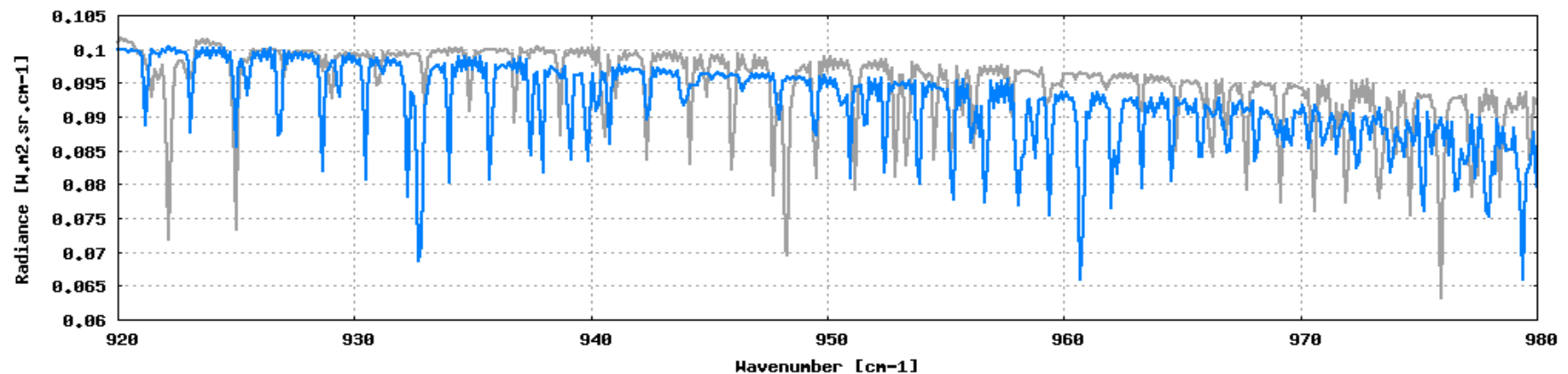
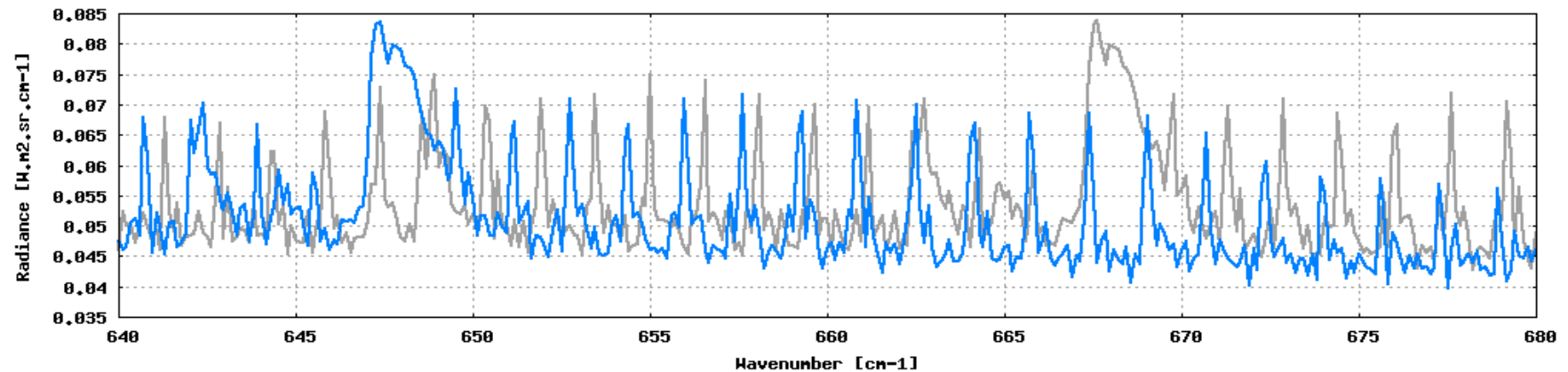
Red: L1C spectrum L1 processing output (real part,  $\text{OPD}_{\text{Max}} = 4 \text{ cm}$ , SRF = L1C)



# Space segment output

Grey: Atmospheric input spectrum ( $\text{Opd}_{\text{Max}} = 4.2 \text{ cm}$ , SRF = Cardinal sine)

Blue: L0 spectrum space segment output (real part,  $\text{Opd}_{\text{Max}} = 4.2 \text{ cm}$ , SRF = Nominal instrument, Background at 80 K)



# Conclusions

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- Since the beginning IASI-NG has been thought as a system including an instrument (INS), on-board processing (OBP), on-ground processing (L1C POP), processing parameters initialisation/monitoring/update (IASTEC).
  - » L1C performances rely on the complementarity and mastering of these 4 components.  
**One fails, all fail !**
- OBP\_Science (and auxiliary data processing): defined and prototyped
  - » First validation done by ADS
- OGP\_Science: defined and prototyped
  - » Scientific validation of algorithms has started (see Adrien's poster #139)
- OGP\_Image: “IASI-like” version has been defined and prototyped
  - » Some improvement with respect to IASI are on-going
  - » Expected to be completed by the end of 2016
- OGP\_ISRFEM: roughly defined and not prototyped yet
  - » Preliminary expected by Q1 2017
- OGP\_TEC : expected by Q2 2018